

Design of reactive power procurement in deregulated electricity market

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Abstract

Reactive power management is required to support real power shipment, providing reserve for voltage security and supplying reactive loads. Reactive power management is different in the deregulated electricity market of various countries. In this paper, a novel reactive power procurement model is proposed, which ensure secure and reliable operation of deregulated electricity market. Various issues of reactive power management in the deregulated electricity market have been discussed. A reactive power bid, reactive capability of a generator has been discussed in the context of procurement reactive power model. A two-level framework of the reactive power is proposed. The first-level of the proposed model, i.e. reactive power procurement, to be done on (few months ahead)advance basis from real time operation with an objective of minimization of reactive generation cost followed by maximization of its Societal Advantage Function(SAF) while considering the second-level, i.e., reactive power dispatch in tandem with real-time operation. The IEEE 24-bus RTS test system is used to illustrate the proposed reactive power procurement. The offers of generation have been considered by minimization of reactive generation cost followed by maximization of Societal Advantage Function.

Keywords: Reactive Bids, Deregulation, Societal Advantage Function, Reactive Power Pricing, Cost of Opportunity Lost(LOC)

1. Introduction

Supply of reactive power has been identified as one of the keys ancillary services in the restructured electricity market. In recently published FERC report (FERC,2005) it is suggested that an efficient pricing and procurement scheme for reactive power should encourage investment in the infrastructure needed to maintain the reliability of the transmission system and provide incentives for the reliable and efficient production and consumption of reactive power from the available infrastructure. In a deregulated electricity market, reactive power provision needs to be made by Independent System Operator (ISO) in order to meet contracted transaction in secure manner (Wang, 2004).

Often the independent generators or local suppliers own the resources for reactive power such as synchronous generators, synchronous condensers, capacitor banks, reactors, Flexible AC Transmission System (FACTS) devices. The reactive power management and payment mechanisms as an ancillary service vary for each deregulated electricity market of various countries in the way the contracts are framed and the markets are operated (Jhong, 2002). For example, the economic formulation has been proposed for optimal power flow real time computation of the reactive power marginal cost (Bhaugman, 1991). A two part reactive power spot pricing scheme is formulated in which one part accounts for investment cost of a new capacitor at a bus and second part is related with the variable spot price which accounts for the operating cost incurred in supplying the additional reactive power from generating units (Bhattacharya, 1995). Total cost of reactive power support is minimized, which includes the explicit cost from various transmission sources such as reactive compensators, tap-changing transformers and opportunity cost from various generation sources (Lemont, 1999).

A novel cost based modified OPF pricing scheme is formulated for reactive power with the assumption that the total reactive power can be divided into two parts. One is for real power transportation when there are no reactive loads in the system and other parts is for reactive power consumption, which is deemed as the responsibility of reactive loads (Dai,2004). The fair and accurate loss allocation scheme for real and reactive power loss was introduced in the bilateral market (Ki, 2006). The pattern of optimal

load dispatch is considered as bi-level problem consisting of an upper and lower part, the upper level problem is that of satisfying the demand functions where the prices are determined by the lower level problem which is basically the optimal power flow problem which has the objective of minimizing the total cost of operating the spatially separated generating units subject to the set of equations that characterize the flow of power throughout the system and all operational constraints (Lin, 2003). Two prices corresponding to real load and reactive load of a consumer has been considered in the context of total cost recovery (Lin, 2005). Reactive power allocation is discussed in a reactive power market (Ki, 2006).

The design of a reactive power procurement model, as discussed in Singh (2010), is as two level approach in which first level is to optimal contracting of reactive power services by the ISO using the maximization of a societal advantage function. In the second level, reactive power dispatches to be close to real time operation.

2. Reactive Power Management in various deregulated electricity markets

There is no generalized reactive power management structure or design yet suggested due to variation of its concepts from one electricity market to another. This is discussed by the same author so only brief part is considered (Singh, 2009). In main countries like USA, UK, Australia, for procurement of reactive power services, the ISO enters into contracts with the reactive power providers. These contracts are usually traditional practices or bilateral agreements as per ISO experience for reactive power support. In the California, provision of reactive power services is based on long-term contracts between CaISO and reliable must-run generators. In Canada, the Independent Electric System Operator (IESO) of Ontario requires generators to operate within a power factor range of 0.9 lag to 0.95 lead and within a $\pm 5\%$ range of its rated terminal voltage. The IESO sign's contracts with generators for reactive power support and voltage control, and generators are paid for the incremental cost of energy loss in the windings due to the increased reactive power generation. The generators are also paid an opportunity cost if they are required to generate reactive power levels by reduction of their real power dispatch. The generator receives payment at the market clearing price (Kirby, 1997). The New York ISO (NYISO) compensate generators based on embedded cost pricing for their reactive power services, and also imposes a penalty for failing to provide reactive power (NY, 1999). In NERC, reactive power provision from generators is mandated within a power factor range 0.9 lagging to 0.95 leading. Beyond these limits, the generators are paid for their reactive power including a loss opportunity cost payment (NERC, 2000).

In UK, the Transmission System Operator (TSO)-National Grid Company (NGC) invites half-yearly tenders from generators for "obligatory reactive power services" which correspond to the reactive power as each generator is required to provide, and "enhanced reactive power services" for generators with excess reactive power capabilities (NGET, 2006).

The payment in Australia (NEMCO, 1999) as follows:

- Availability Payments: All reactive support providers are eligible for the *availability payment component* for their preparedness to provide the service when called for.
- Enabling Payment: Synchronous compensators also receive the *enabling payment component*- paid when their service is activated by the ISO for use.
- Usage Payment: Based on actual use. Such as rapid loading and unloading services of generators.
- Compensation Payment: On the other hand, a generator receives the *compensation payment component*- which is based on its opportunity cost.

In the Sweden, contrary to other countries, reactive power services are provided on a mandatory basis from the synchronous generator, and so no financial compensation is provided.

Procurement of reactive power services through competition and long-term contracts between the ISO and service providers (generators) is an alternate way for reactive power management in deregulated electricity markets (Zhong, 2000, 2002). Reactive power market has been considered more as a local market than a system-wide market (Zhong, 2004).

The present work extends the issue to the creation of a competitive market for reactive power services on the long term basis and illustrates proposed model with IEEE 24-bus test system. Short term framing concept is derived but due to paper limitation, it is not discussed in detail.

3. Framework of Reactive Power Provision

Reactive power provisions can also be framed as two classes of a problem in the context of deregulated electricity markets, namely,

- Reactive power procurement and
- Reactive power dispatch.

Reactive power procurement is basically a long-term issue, i.e., a seasonal problem; in this case, the ISO obtains optimal reactive power "allocations" from possible suppliers that would be best suited to its needs and constraints in a given season [El.Samahy, 2001]. This optimal set would be determined based on forecasts of the demand and system conditions expected over the planning horizon. The criterion for such procurement could be varied, but would essentially consider the cost/price offers of reactive power provision. This long term procurement can be done assuming like 60 days ahead on a season basis. The second level in the

proposed approach to a reactive power provision is the short-term management function, which takes place one to half hour ahead of real-time.

A reactive power management scheme based on reactive power procurement versus its real time dispatch is proposed that comprises two major time-based steps (shown in Figure 1).

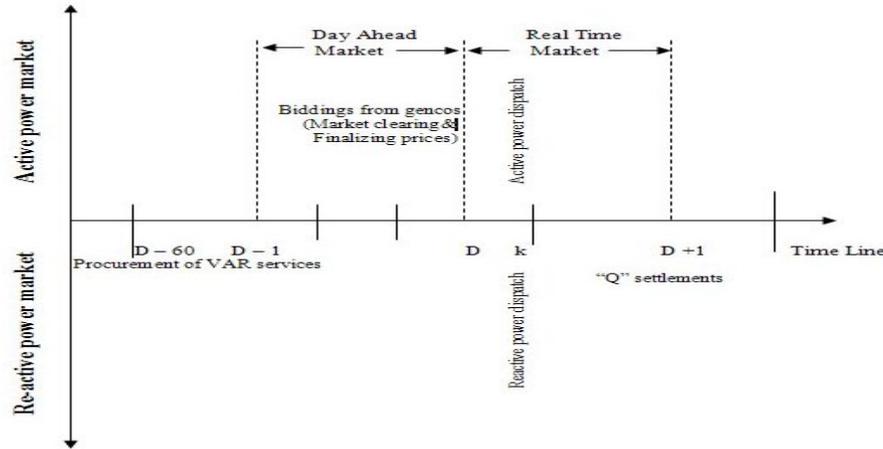


Figure1. Electricity market clearing and dispatch at day D hour k.

The Electricity market settlement is decoupled into two sub-problems as active and reactive OPF sub-problem of market settlement to avoid coupled market complexity. Active power sub-problem market provides real-time based the active power prices and dispatches with cost minimization along-with their social welfare maximization. Reactive power sub-problem market model provides reactive power levels and prices based on a taken optimization criterion operating in different time frames. A required flexibility for spot market application is provided by decoupling OPF problem retaining a sufficient level of accuracy. Figure 1 describes decoupling of active and reactive power markets keeping these two markets in entirely different operating time frames, so that the ISO does not entertain reactive power management in the same time frame as that of real power auctions. This basically reduces market inefficiencies and minimizes the risk that might arise from price volatility of real power.

3.1 Reactive Power Procurement

In the reactive power procurement, first reactive power offers from the reactive power providers are called and based on the received bids. An optimization model is solved, which maximizes a societal welfare function subject to system constraints. This optimization model yields the required reactive power service “reserves” for each generator along with the price components of reactive power. The selected providers would be receiving an availability payment for these reserves as a long-term obligation for the reactive power provision. The schematic representation of reactive power procurement in long term management mechanism is depicted in Figure 2.

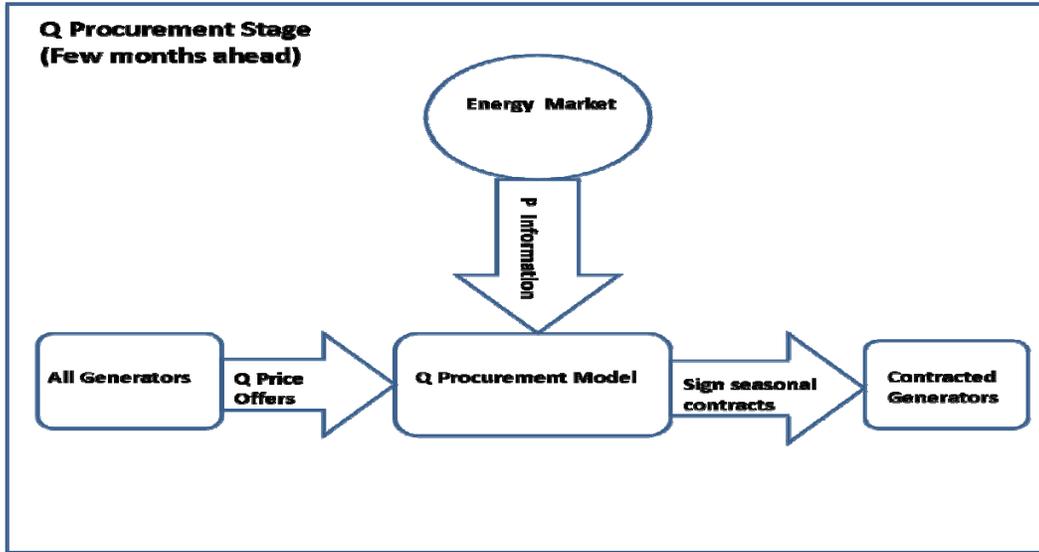


Figure 2. Long term management for Reactive Power Services

3.1.1 Reactive Power limits of Synchronous Generator

The point of intersection of the two curves formed with armature and field winding heating limits decides MVA rating of Synchronous Generator. The armature heating limit is taken in circle form with $R_1 (=V_t I_a)^{1/2}$ radius, centre on $C_1(0, 0)$. The field heating limit also forms a circle with $R_2 (=V_t E_{af} / X_s)$ radius, centre on $C_2(0, -V_t^2 / X_s)$. (as shown in figure3)

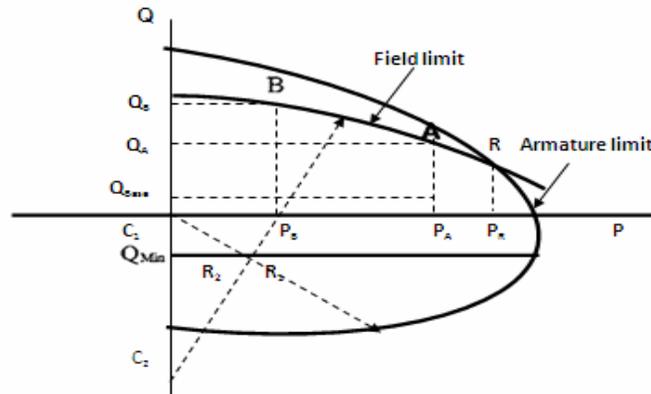


Figure3. Determination of Reactive Power limits from Generators

As per the capability curve (as shown in Figure 3), the generator requires minimum Q_{Base} for its auxiliary equipment. The generator may increase its reactive generation from Q_{Base} up to Q_A without requiring readjustment of P_A , If the operating point says, at (P_A, Q_{Base}) lies inside the limiting curves. However, this will result in increased losses in the windings and so cost of losses increases. Any increase in Q beyond the limiting curve will require a decrease in P to adhere to field heating limits as per capability curve. Consider the operating point 'A' on the curve (P_A, Q_A) , the operating point requires shifting back along the curve to point $B(P_B, Q_B)$, where $P_B < P_A$. This signifies that the unit has to reduce its real power output to adhere to field heating limits when higher reactive power demanded. Due to the reduced production of real power, loss in revenue is termed loss opportunity cost.

So three operating regions for a generator are defined, which are as follows:

Region-1: (When $Q_G=Q_1$ lies between 0 and Q_{min})

It means the generator is absorbing reactive power within this region. It would incur a cost of loss for absorption.

Region-2: (When $Q_G=Q_2$ lies between Q_{Base} and Q_A)

Mandatory lagging behind reactive power is from 0 to Q_{Base} . It means that generator is injecting reactive power and so entitled for payment for the increased losses in the winding (Cost of loss component).

Region-3:(When $Q_G=Q_3$ lies between Q_A and Q_B)

Generator will be required to decrease active power generation and so eligible for cost payment of loss of opportunity.

3.1.2 Structure of Reactive Power Offers from Generator:

Based on the classification of reactive power production costs, an offer structure can be formulated (also shown in figure4.)

- Availability price offer (a_0 , \$/h): A fixed component to account for that portion of a supplier’s capital cost that can be attributed to reactive power production.
- Cost of the loss offer (m_1 , m_2 , \$/MVAR-h): An assumed linearly varying component to account for the increased winding losses as reactive power output increases, in the under- and over- excitation ranges, respectively.
- Opportunity offer (m_3 , \$/MVAR-h/MVAR-h): A quadratic component to account for the lost opportunity cost when a supplier is constrained from producing its scheduled real power in order to increase its reactive power production.

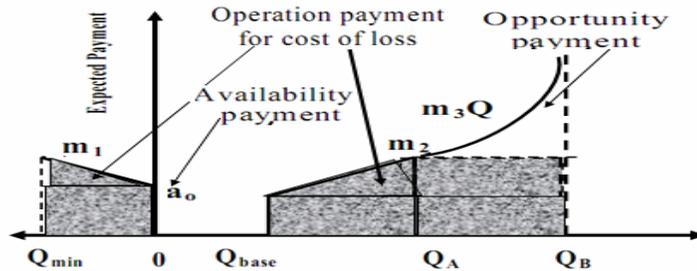


Figure 4. Reactive power offer structure of a generator

3.1.3 Marginal Benefit of Reactive Power Supply from Synchronous Generator:

Reactive Power output from a provider is classified into three regions ($Q_{min}, 0$), (Q_{Base}, Q_A) and (Q_A, Q_B). It is considered as three components: Q1, Q2 or Q3 respectively and generator will provide their respective offer bids. Accordingly, only one of the binary variables W_1, W_2 or W_3 can be selected. The opportunity cost for Q3 is quadratic function as shown in figure 4. Using the elementary mathematics we can derive the following cost function:

To minimize:

$$Cost = \sum_{i=1}^{NG} \sum_{h=1}^{NH} (\rho_0 \cdot W_{0,i,h} - \rho_1 \cdot W_{1,i,h} \cdot Q_{1,i,h} + \rho_2 \cdot W_{2,i,h} (Q_{2,i,h} - Q_{base,i,h} + \rho_2 \cdot W_{3,i,h} (Q_{3,i,h} - Q_{base,i,h}) + \frac{1}{2} \rho_3 \cdot W_{3,i,h} [(Q_{3,i,h}^2) - (Q_{A,i,h}^2)]) \tag{1}$$

In eqn (1), if any generator is selected then $W_{0,i,h}$ will be 1 irrespective of its amount of reactive power output.

$W_{1,i,h}, W_{2,i,h}$ and $W_{3,i,h}$ are binary variables i.e. $[(W_{1,i,h}, W_{2,i,h}, W_{3,i,h}) \in \{0,1\}]$.

If h^{th} supplier connected to i^{th} bus is selected then $W_{0,i,h}$ will be equal to one so only one of the binary variables

$W_{1,i,h}, W_{2,i,h}$ or $W_{3,i,h}$ will be selected. It means only then

$$W_{1,i,h} + W_{2,i,h} + W_{3,i,h} = 1$$

NG is group of generator and NH is representation of each supplier at a bus.

$Q_{1,i,h}, Q_{2,i,h}$ and $Q_{3,i,h}$ represent the regions($Q_{min,i,h}$ to 0),($Q_{base,i,h}$ to $Q_{A,i,h}$)and ($Q_{A,i,h}$ to $Q_{B,i,h}$) i.e.

$$Q_{i,h} = Q_{1,i,h} + Q_{2,i,h} + Q_{3,i,h}$$

The system constraints are as follows:

The equality constraints of the OPF problem are as follows:

$$\sum_{h=1}^{NH_i} P_{G,i,h} - P_{Di} - \sum_{j \in N} |V_i| |V_j| |Y_{ij}| \cos(\theta_{ij} + \delta_j - \delta_i) = 0; \forall i, h \in NG \quad (2)$$

$$\sum_{h=1}^{NH_i} Q_{G,i,h} - Q_{Di} - \sum_{j \in N} |V_i| |V_j| |Y_{ij}| \sin(\theta_{ij} + \delta_j - \delta_i) = 0; \forall i, h \in NG \quad (3)$$

Where N is the total number of buses in the system;

$P_{Gi}, Q_{Gi}, P_{Di}, Q_{Di}$ are the active and reactive power generation and demand on bus i .

$Y_{ij} \angle \theta_{ij}$ is the element in the bus admittance matrix. $\dot{V} = V_i \angle \delta_i$ is the bus voltage at bus i .

The inequality constraints are:

1. Generation limits:

$$P_{Gi, \min} \leq P_{Gi} \leq P_{Gi, \max} \quad i \in G \quad (4)$$

2. Reactive limits:

$$Q_{Gg} \leq Q_{Gg}^{\max}, \forall g$$

Where

$$Q_G^{\max} = \sqrt{(V_t E_{af} / X_s)^2 - (P_G)^2} - V_t^2 / X_s \quad \text{for } P_G < P_R \quad (5)$$

$$\text{or } \sqrt{(V_t I_a)^2 - (P_G)^2} \quad \text{for } P_G > P_R$$

$$Q_{Gg} \geq Q_{Gg}^{\min}, \forall g \quad (6)$$

3. Voltage Limits

$$V_{i, \min} \leq |V_i| \leq V_{i, \max}, \forall i \quad (7)$$

4. Transmission Limits:

$$|P_{ij}| \leq P_{ij, \max} \quad i \neq j \text{ and } \forall i, j \quad (8)$$

Where

$$P_{ij} = |V_i| |V_j| |Y_{ij}| \cos(\theta_{ij} + \delta_j - \delta_i) - |V_i|^2 |Y_{ij}| \cos \theta_{ij}$$

5. The constraints of generators for reactive power compensation

$$W_{2,i,h} \cdot Q_{base,i,h} \leq Q_{2,i,h} \leq W_{2,i,h} \cdot Q_{A,i,h} \quad (9)$$

$$W_{3,i,h} \cdot Q_{A,i,h} \leq Q_{3,i,h} \leq W_{3,i,h} \cdot Q_{B,i,h} \quad (10)$$

$$W_{1,i,h} + W_{2,i,h} + W_{3,i,h} \leq 1 \quad (11)$$

$$W_{1,i,h} + W_{2,i,h} + W_{3,i,h} = W_{0,i,h} \quad (12)$$

6. Constraints for determination of uniform price offers of generators

$$W_{0,i,h} \cdot a_{0,i,h} \leq \rho_0; \forall i, h \in NG \quad (13)$$

$$W_{1,i,h}.m_{1,i,h} \leq \rho_1 \forall i, h \in NG \quad (14)$$

$$(W_{2,i,h} + W_{3,i,h}).m_{2,i,h} \leq \rho_2 \forall i, h \in NG \quad (15)$$

$$W_{3,i,h}.m_{3,i,h} \leq \rho_3 \forall i, h \in NG \quad (16)$$

In the above equations, Eqn (1) is cost minimization, eqn, Eqn (2) - (3) are considered as equality constraints of power balance equations. Eqn (4) to (8) are taken as inequality constraints and from eqn (9) to (16) are constraints of a generator for reactive power compensation and constraints for determination of uniform zonal price offers.

The basic cost function is referred from J. Zhong[3, 18,19,20] , Bhattacharya [5], El-Samahy[21,22] , Rabiee et al. (2009). In this paper their work has been extended and social welfare function is used for procurement of reactive power in long term market.

As mentioned above, reactive power procurement model is formed based on the marginal contributions of reactive power from generation cost minimization. In the result, the Lagrange multipliers that represent the marginal benefit/contribution of each reactive power source with respect to reactive cost minimization are λ_g, γ_g and μ_g . λ_g denotes the sensitivity of the objective function to a change in system demand. Simply stated λ denotes the change in the system cost for a 1MW in the system demand. The multiplier μ and γ are associated with the generator limits and these are of significance only when a generator limit is a binding constraint. An important point can be stated here is that when the generating limit is not binding then $\mu=0$ and $\gamma=0$. All the three Lagrange multipliers will be zero for any generator as long as it lies within the limits specified, whereas will be a nonzero value for any generator if its touches the upper or lower limits of the respective region.

3.1.4 Societal Advantage Function

Once the reactive power, ancillary service limits and the marginal benefits of each provider with respect to reactive generation cost are determined, and reactive power offers are received, the ISO is in a position to carry out a procurement market settlement where its sole objective is to maximize a societal advantage function. The proposed SAF is formulated considering benefits accrued from reactive power services with respect to expected payment by the ISO. SAF is considered on a zonal basis and can be expressed as follows:

$$\begin{aligned} SAF_K = & -\sum_{g \in K} \rho_{0K} + \sum_{g \in K} (c_L \mu_g - \rho_{1K}) Q_{1g} + \sum_{g \in K} (c_L \lambda_g - \rho_{2K}) (Q_{2g} - Q_{baseg}) \\ & + \sum_{g \in K} ((c_L \gamma_g - \rho_{2K}) (Q_{3g} - Q_{baseg}) - 0.5 \rho_{3K} [(Q_{3g} - Q_{Ag})^2] \end{aligned} \quad (17)$$

In (9), the the subscript g denotes set of generators in the zone K considering that the system is divided into zones. The variables ρ_{1k} (in \$/MVar-h) and ρ_{2k} (in \$/MVar-h) are the under- and over-excitation prices for reactive power in the zone k, respectively; similarly ρ_{3k} (in \$/MVar-h/MVar-h) is the zonal uniform opportunity price component. The variable ρ_{0k} (in \$) is the zonal availability price component. The constant C_L is a "loadability" cost parameter (in \$/MWh) denoting the economic worth of increasing the system loadability. It is taken as 100\$/MWh in this paper.

The proposed procurement algorithm is based on the following OPF model:

Maximize SAF as given in eqn (17) with following constraints

- 1) Load flow (2), (3)
- 2) Reactive Power Generation limits (4), (5), (6)
- 3) Bus Voltage limits (7)
- 4) Power Transfer limit (8)
- 5) The constraints of generator (9), (10), (11), (12) and
- 6) Constraints for price offer (13), (14), (15), (16).

The solution of the above procurement model yields the set of contracted generators as well as the zonal uniform price components after its maximization of societal advantage function.

3.2 Reactive Power Dispatch

The second level in the proposed hierarchical approach to reactive power management is the short-term management function, which takes place one to half hour ahead of real-time. The real-time dispatch of reactive power only takes into account the current operating conditions, with the ISO arriving at the optimal dispatch via an OPF (shown in Figure5). Based on actual usage and actually dispatch requested, cumulative payment to a supplier is calculated post real time operation.

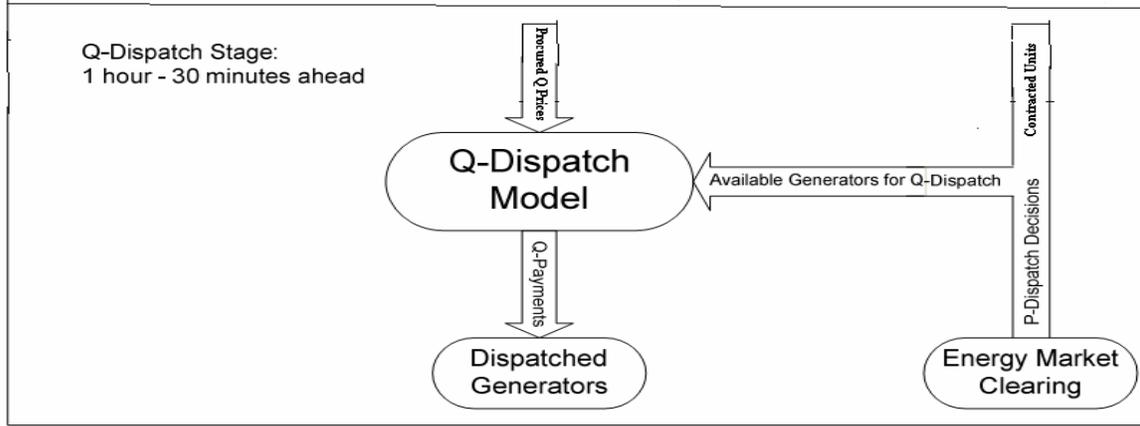


Figure5. Reactive power dispatch (short term management)

4. Maximization of Societal Advantage Function in Reactive Power Procurement

It is important to mention that the solution for above problem formulation is Non Linear Programming solution. The main objective is to choose only one region of reactive power operation to satisfy the conditions associated with the quadratic term and the constraints. λ , γ and μ are the Lagrange multipliers obtained from the optimization model of marginal benefits of reactive power supply. Final optimization is done to maximize Societal Advantage Function in terms of ISO to provide high performance contribution to the system from generators with minimum payment burden. The flow chart for SAF is as follows:

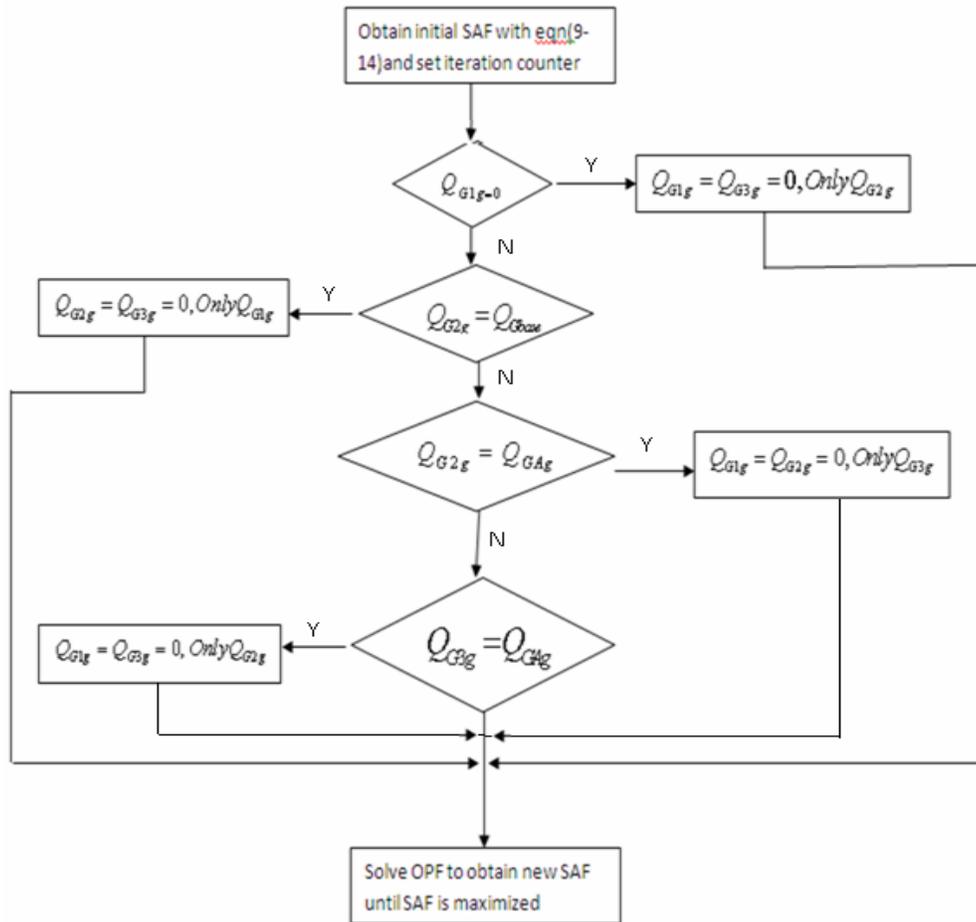


Figure 6. Maximization of SAF with reactive power procurement

The objective is to maximize SAF based on values found of λ , γ and μ alongwith values of Q1, Q2 and Q3. At first initial SAF is calculated. For generator, check if Qg hits the limits in any region like if Qg= Qg_{2max} of region II then considers Qg in region III and resolve SAF-optimization eqn(9 to 14).This way updation is applied with the condition that SAF is maximized.

5. Implementation and Results

The simulation is performed in the Matlab. The input parameters are given in nomenclature.The results in terms of marginal benefit are shown in Table 1 and final results are shown in Table 3. Reactive power procurement scheme is tested on the IEEE 24 bus (RTS) system [IEEE RTS] shown in figure7. There are 32 synchronous generators, 1 synchronous condenser (located at bus 14) and 17 constant –power type loads. The participants of decoupled reactive power market are supposed to submit their four components of the offer prices (a0, m1, m2, m3) (Rabiee, 2009). The participants are also required to send their Q_{min} , Q_{Base} , Q_{max} .In this paper, $Q_{base} = 0.1 \times Q_{max}$ and $Q_A = 0.8 \times Q_B$ are considered. This is a non-linear programming (NLP) problem. The simulation is performed in Matlab. In this paper, Fmincon is used to solve nonlinear constrained objective. Fmincon is an optimization tool in Matlab. Fmincon attempts to find a constrained minimum of a scalar function of several variables starting at an initial estimate. This is generally referred to as constrained nonlinear optimization or nonlinear programming. Fmincon finds the minimum of constrained nonlinear multivariable function. Fmincon minimizes the function of more than one variable subject to constraints that the specified function of the solution should be positive or zero. The first step is to calculate λ , γ and μ for each generator by solving the OPF model. All Qg values are in p.u. with respect to a base value of 100 MVA.

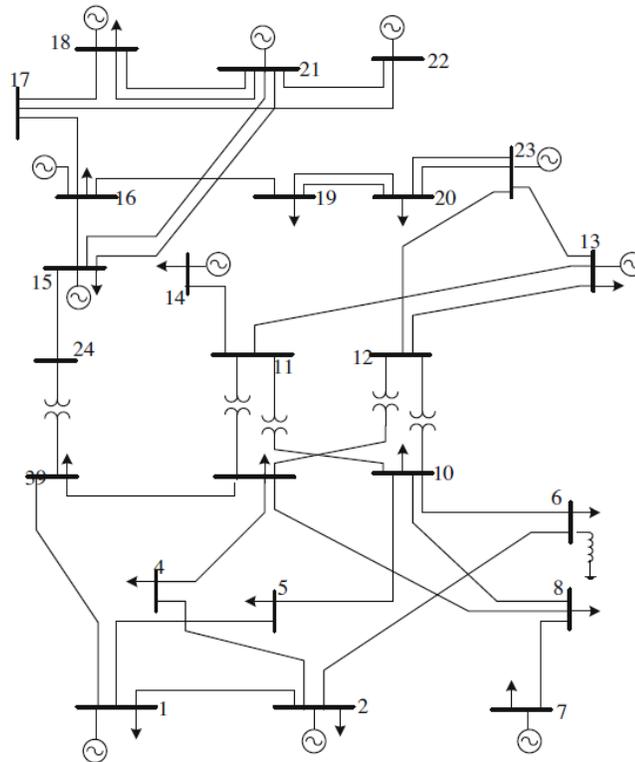


Figure 7. IEEE 24-Bus RTS system

Table 1 shows offer data for all the generators. The solution is given in Table 2. It is clear that Qg can only take one of the three values corresponding to the region of operation of respective generator and so regions are shown in the Table 2. The second step is to solve OPF that maximizes Societal Advantage function using values of first step and Qg. The final solutions of OPF problem are given in Table 2, where the total cost payment to generators is given along with final price offers as uniform availability price, under-excitation price and over-excitation price respectively. The optimal value of the objective function S_w is 134 \$.

Table 1: Reactive Power contract offer prices of 24 Bus (RTS) IEEE system

Bus no.	Unit no.	$a_0^{i,u}$ (\$)	$m_1^{i,u}$ (\$/MVar-h)	$m_2^{i,u}$ (\$/MVar-h)	$m_3^{i,u}$ (\$/MVar-h/MVar-h)
1	1	0.96	0.86	0.86	0.46
1	2	0.94	0.82	0.82	0.45
1	3	0.85	0.79	0.79	0.39
1	4	0.83	0.82	0.82	0.40
2	1	0.50	0.54	0.54	0.28
2	2	0.42	0.42	0.42	0.35
2	3	0.69	0.68	0.68	0.39
2	4	0.65	0.62	0.62	0.37
7	1	0.75	0.61	0.61	0.43
7	2	0.80	0.75	0.75	0.36
7	3	0.70	0.65	0.65	0.32
13	1	0.68	0.50	0.50	0.31
13	2	0.70	0.54	0.54	0.39
13	3	0.75	0.60	0.60	0.50
14*	1	0.94	0.81	0.81	0.00
15	1	0.65	0.60	0.60	0.30
15	2	0.50	0.58	0.58	0.25
15	3	0.60	0.73	0.73	0.38
15	4	0.55	0.61	0.61	0.27
15	5	0.52	0.50	0.50	0.26
15	6	0.51	0.51	0.51	0.27
16	1	0.50	0.50	0.50	0.30
18	1	0.90	0.85	0.85	0.48
21	1	0.80	0.75	0.75	0.41
22	1	0.42	0.42	0.42	0.17
22	2	0.50	0.48	0.48	0.20
22	3	0.45	0.42	0.42	0.38
22	4	0.48	0.44	0.44	0.35
22	5	0.49	0.45	0.45	0.33
22	6	0.55	0.46	0.46	0.32
23	1	0.90	0.85	0.85	0.48
23	2	0.95	0.89	0.89	0.55
23	3	0.86	0.80	0.80	0.45

* Synchronous Condenser (SC)

Table 2: After Cost minimization, the values of λ , γ , μ and Q_G

Buses having Generators	Lagrange multipliers from cost minimization			Q_G	Classification of regions of Q_G			Q_G^{\max}	Q_G^{\min}
	λ	γ	μ		Q_1	Q_2	Q_3		
1	.04961	.049589	0	4.07709	0	4.07709	0	10	0
1	.04961	.049587	0	4.07709	0	4.07709	0	10	0
1	.04961	.049588	0	-0.78852	-0.78852	0	0	30	-25
1	.04961	.049588	0	-0.78852	-0.78852	0	0	30	-25
2	.05085	0	.049687	8.640155	0	8.640155	0	10	0
2	.05085	0	.049687	8.640155	0	8.640155	0	10	0
2	.05085	0	0	-6.752158	-6.752158	0	0	30	-25
2	.05085	0	0	-6.752158	-6.752158	0	0	30	-25
7	.050398	.05112	0	16.43847	0	16.43847	0	60	0
7	.050398	.05112	0	16.43847	0	16.43847	0	60	0
7	.05039	.05112	0	16.43847	0	16.43847	0	60	0
13	.05017	0	0	32.59147	0	32.59147	0	80	0
13	.05017	0	0	32.59147	0	32.59147	0	80	0
13	.05017	0	0	32.59147	0	32.59147	0	80	0

Table 2 (cont'd): After Cost minimization, the values of λ , γ , μ and Q_G

Buses having Generators	Lagrange multipliers from cost minimization			Q_G	Classification of regions of Q_G			Q_G^{\max}	Q_G^{\min}
	λ	γ	μ		Q_1	Q_2	Q_3		
15	.04780	0	.048045	6	0	0	6	6	0
15	.04781	0	.048045	6	0	0	6	6	0
15	.04781	0	.048045	6	0	0	6	6	0
15	.04781	0	.048045	6	0	0	6	6	0
15	.04781	0	.048045	6	0	0	6	6	0
15	.04781	0	.048045	80	0	0	80	80	-50
16	.045239	0	.050851	80	0	0	80	80	-50
18	.04756	0	.046575	72.898438	0	72.898438	0	200	-50
21	.0489983	0	0	-7.458590	-7.458590	0	0	200	-50
22	.0495877	.04783	0	-6.413298	-6.413298	0	0	16	-10
22	.0495877	.04783	0	-6.413298	-6.413298	0	0	16	-10
22	.0495877	.04783	0	-6.413298	-6.413298	0	0	16	-10
22	.0495877	.04783	0	-6.413298	-6.413298	0	0	16	-10
22	.0495877	.04783	0	-6.413298	-6.413298	0	0	16	-10
22	.0495877	.04783	0	-6.413298	-6.413298	0	0	16	-10
23	.0510717	.05181	0	11.957806	0	11.957806	0	80	-50
23	.0510717	.05181	0	11.957806	0	11.957806	0	80	-50
23	.0510717	.05181	0	21.727909	0	21.727909	0	150	-25

Table 3: Final reactive power offer prices and generator reactive power cost payment

Generator Payment cost after its cost minimization (\$/h)	6.3352e+004
Availability price(ρ_0)(MCP for a_0) in\$	0.96
Under-excitation price(ρ_1)(MCP for m_1) in\$/MVAh	0.89
Over-excitation price(ρ_1)(MCP for m_2) in \$/MVAh	0.89
Opportunity price (ρ_3)(MCP for m_3) in \$/MVAh/MVAh	0.00

6. Conclusions

The main objective of this paper is to design reactive power procurement market model in a deregulated electricity market. The proposed market design consists of two stages, namely, procurement of reactive power from generators on a long term(few month ahead) basis, and a real-time reactive power dispatch (short term stage)which is done in tandem with real time market. The main focus of this paper is a reactive procurement market model, which is a basically two-step optimization process. The first step determines marginal benefits of reactive power with respect to reactive generation cost considering all equality and inequality constraints. Results are then used in the second step to maximize a reactive power societal advantage function (SAF) considering bids from each service provider. In the second level, reactive power dispatch be close to real time operation. Result gives set of generators & uniform price offers that would form a basis of contractual agreement for a reactive power provision with maximization of societal advantage function. In the future we are planning to extend this work for different operating conditions and loading parameters.

Nomenclature

Symbol	Description	Value
$P1k$ (in \$/MVAh)	over-excitation prices for reactive power in zone k	
$P2k$ (in \$/MVAh)	under-excitation prices for reactive power in zone k	
$P3k$ (in \$/MVAh/MVAh)	zonal uniform opportunity price component	
ρ_k (in \$/h)	zonal availability price component	
C_L (in \$/MWh)	economic worth of increasing the system loadability	100 input parameter
Q_{Gg} in p.u.	Reactive power generation of generator at bus g	
P_{Gg} in p.u.	Active Power generation at bus g	
V_t in p.u.	Terminal voltage of generator g at which its capability curves are calculated	input parameter
E_{af} in p.u.	Excitation voltage of generator g in p.u	input parameter
X_s	Synchronous reactance of generator g	input parameter
$V_{i,min}$	Minimum allowable voltage at bus i	input parameter
$V_{i,max}$	Maximum allowable voltage at bus i	input parameter
λ_g	Dual of the reactive power balance constraint (3)	
γ_g	Dual of reactive power constraint of generator (5)	
μ_g	Dual of the under-excitation constraint (6)	
P_r	Reactive power prices	input parameter
P_r	Rated power of the generator	

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