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EFFECT OF HNO₃ TREATED TIO₂ ON STRUCTURAL AND ELECTRICAL PROPERTIES OF HEXANOYL CHITOSAN/POLYSTYRENE-LICF₃SO₃-TIO₂ COMPOSITE POLYMER ELECTROLYTES

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ABSTRACT

In searching for solutions to reduce battery weight for military applications, films of composite polymer electrolytes comprised of hexanoyl chitosan/polystyrene containing lithium trifluoromethanesulfonate (LiCF₃SO₃) and titanium oxide were prepared using solution casting technique. Two types of TiO₂ filler were used, which are untreated TiO₂ and HNO₃-treated TiO₂. The effect of untreated and HNO₃-treated TiO₂ on the structural and electrical behavior of the prepared electrolyte systems has been investigated by using X-ray diffraction and impedance spectroscopy, respectively. The ac conductivity was calculated using $\sigma(\omega) = \sigma_{dc} + A\omega^s$ formula in the temperature range from 283 K to 353 K. The conduction mechanism of H-chitosan/PS-LiCF₃SO₃-TiO₂ the and H-chitosan/PS-LiCF₃SO₃-HNO₃-treated TiO₂ can be interpreted based on the correlated barrier hoping model at 4 and 6 wt.% of TiO₂ respectively.

Keywords: hexanoyl chitosan; polystyrene; composite polymer electrolytes.

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1. INTRODUCTION

While able to benefit from technology, the army is facing a number of challenges in their operations today and in the future. One of the major challenges is in the power sources arena. Today's soldier carries a wide array of electronic devices such as computers, communications equipment, weapon system and all requiring portable power. The army is aware of the situation and has identified problem areas of battery weight, space and power source carried by the soldier [1]. One area identified to further study is the electrolyte for battery system using polymer electrolyte. Polymer electrolyte offers reduction in size, weight and thermal management properties in line with the requirement of future military systems. With better process efficiency, the batteries can be designed to be lighter in weight hence reducing the operational physical load of soldiers which may contributes to longer endurance and reduce fatigue during operations.

Polymer electrolytes are of immense interest due to their applicability in energy conversion and storage devices. They present significant advantages over liquid electrolytes such as safer design, simpler stacking and hermetic sealing processes, superior in density, flame-resistance and shape suitability in the requirements of the application [2-3]. In order to achieve high performance, a battery electrolyte must possess high ionic conductivity, be stable at both the high potential of the battery cathode and the low potential of the battery anode. Various approaches to enhance the ionic conductivity of polymer electrolytes have been suggested in the literature such as by addition of plasticizer, filler and blending polymer [4-5]. The recent technique developed for solid polymer electrolyte is the dispersion of nano-size inorganic ceramic filler particles such as Al₂O₃, SiO₂, TiO₂, SnO₂, ZnO and ZrO into the polymer electrolytes system called composite polymer electrolytes (CPE). It has been shown that the addition of fillers to semicrystalline PEO-alkali metal salt complexes leads to the decrease in the crystallinity of the electrolyte and enhancement in ionic conductivity [6]. Also, the uses of fillers improve mechanical stability of the polymer electrolytes. Changes in the ionic conductivity of CPEs result from the Lewis acid-base interactions between the fillers and the polymer electrolytes components.

From ac conductivity, further information on ionic conduction model can be determined to get

more insight on ion conduction mechanism. Various models reported such as small polaron tunneling model (SPT) overlapping large polaron tunneling model (OLPT), correlated barrier hopping model (CBH) and quantum mechanical tunneling model (QMT) have been reported to discuss the ac conduction mechanism in amorphous materials such as semiconductors and glasses [7]. However, there are limited researches available regarding the use of such models to explain the ionic conduction mechanism in polymeric materials.

In order to obtain a balance for the compatibility of filler and polymer electrolytes, several investigations have been carried out such as synthesis of new polymer matrix, preparation of polymer single-ion conductor and doping with filler. Thus, in this research we prepared blended based polymer of hexanoyl chitosan and polystyrene doped with LiCF_3SO_3 . Two types of TiO₂ filler were used, which are untreated TiO₂ and HNO₃-treated TiO₂. The effect of untreated and HNO₃-treated TiO₂ will be investigated on their ionic conductivity, crystalline fraction, dielectric constant and ionic conduction model.

2. RESULTS AND DISCUSSION

A structural study of solid polymer electrolyte was investigated by XRD. XRD analysis was performed to determine the degree of crystallinity and to observe the glassy nature of the H-chitosan/PS polymer electrolyte.

The degree of crystallinity in the prepared samples were estimated from the ratio of integrated intensity of the peak at $2\theta \approx 6.86^{\circ}$ to the total integrated of the spectrum, using the Equation (1)

$$X_C = \frac{I_C}{I_T} \tag{1}$$

where X_C is the degree of crystallinity, I_C is the $2\theta \approx 6.86^\circ$ peak intensity and I_T is the total integrated intensity.

Fig. 1 shows the variation in the degree of crystallinity as a function of untreated and treated TiO₂ concentration. The crystallinity degree was estimated from the peak at $2\theta \approx 6.86^{\circ}$ using the same method as discussed previously [9]. It can be observed that for both the untreated and treated TiO₂-added electrolyte system, the degree of crystallinity decreases with addition of TiO₂ up to 6 wt.% which is from 19.62% to 13.52 and 14.43% respectively. The reduction

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polymer [10]. At 8%, the crystallinity of H-chitosan/PS increases drastically to 22.34%. This indicates that 6 wt.% of TiO_2 is the optimum amount and beyond this weight percentage, the presence of TiO_2 leads to recrystallization of H-chitosan/PS. This observation will be supported with ionic conductivity as discussed below.



Fig.1. The variation in crystalline fraction for composite electrolyte system as a function of (a) untreated TiO₂ and (b) HNO₃-treated TiO₂ concentration

The variation of room temperature conductivity as a function of untreated and treated TiO₂ concentration is depicted in Fig. 2. The ionic conductivity of H-chitosan/PS electrolytes without TiO₂ filler was 7.21×10^{-5} S cm⁻¹. With addition of 2 wt.% TiO₂, the ionic conductivity of both the untreated and treated TiO₂ systems decreases to around 7.00×10^{-6} and 5.86×10^{-6} S cm⁻¹. Small amount of filler was not able to overcome the rate of ion association of LiCF₃SO₃. The conductivity increases with further increase in filler content, reaches a maximum and thereafter decreases with increasing filler content beyond the optimum concentration. The maximum conductivity achieved was 2.27×10^{-4} S cm⁻¹ at 4 wt.% for untreated TiO₂ and 1.47×10^{-4} S cm⁻¹ at 6 wt.% for HNO₃-treated TiO₂ only half compared to without filler. The conductivity enhancement is due to presence of oxygen sites as conduction pathways from TiO₂, hence help to increase in the number of mobile Li⁺ cation. However, HNO₃-treated TiO₂ systems produce lower ionic conductivity compared to untreated TiO₂ systems because treated TiO₂ have more acidic sites that help to increase the

degree of ion association. Treated TiO_2 decreased the conductivity by decreasing the anionic contribution due to the HNO₃-treated TiO_2 grain surface consists of solely OH group and it shown that anion of salt has larger affinity towards filler surface acid site than cation as reported in our previous work [11]. At 10 wt.% TiO_2 , the ionic conductivity decreases significantly even below the unfilled electrolytes. This behavior is due to the recrystallization of polymer host as observed in XRD analysis. The conductivity variations observed also could be attributed to the variation in the number of free ions in the samples. This is reflected in the dielectric constant, ε r versus frequency curves as illustrated in Fig. 4.





TiO₂ concentration at room temperature (a) untreated TiO₂ and (b) HNO₃-treated TiO₂ Fig. 3 represents the plot of ionic conductivity (log σ) versus the inverse absolute temperature for untreated and HNO₃-treated TiO₂ electrolyte system respectively. The measurement was carried out from 283 K to 383 K. Within the temperature range investigated, the variations of log σ with 1/T are linear with R² = 0.953 and 0.985 for untreated TiO₂ and HNO₃-treated TiO₂. This indicates that the conductivities of the studied electrolyte systems are thermally activated which indicating that this system obeyed the Arrhenius rule [12]. Therefore, as temperature was increased, the number of free lithium ions was also increased. Hence, it increases the conductivity of the electrolytes [13]. The graph shows that conductivity 4 wt.% untreated TiO₂ is higher than 6 wt.% HNO₃-treated TiO₂. Activation energy, E_a for ionic conduction were obtained from the slope of the plots in Fig. 3 and E_a for 4 wt.% untreated TiO₂ and 6 wt.% HNO₃-treated TiO₂ was 0.048 and 0.096 eV. E_a is the energy required for an ion to begin migration from one donor site to another. This ion migration results in conduction. It can be observed that high conducting sample exhibits low value of E_a . This indicates that ions in high conducting sample require lower energy to begin migration.



Fig.3. Temperature dependence of conductivity for H-chitosan/PS-LiCF₃SO₃ with a) 4 wt.% untreated TiO₂ and b) 6 wt.% HNO₃-treated TiO₂

The dielectric constant represents the stored charge in a material. Since charge is carried by ions, therefore it can be deduced that the increase in dielectric constant reflects the increase in the number of ions [14]. Fig. 4 shown frequency dependence of dielectric constant, ε_r for H-chitosan/PS-LiCF₃SO₃ with untreated TiO₂ and HNO₃-treated TiO₂. The untreated TiO₂ system has higher dielectric constant value than HNO₃-treated TiO₂ system. This suggests that the untreated TiO₂ system has higher conductivity. The calculated number of mole of H⁺ for untreated TiO₂ system and leading to higher conductivity. The calculated number of mole of H⁺ for untreated and HNO₃-treated TiO₂ are 6.11×10^{-5} and 7.40×10^{-4} mol/g respectively. The acidic H⁺ site acts as anion trapper [15]. The treated TiO₂ possesses more H⁺ anion trapper on its surfaces compared to untreated TiO₂. The reduce number of free anions in the system contribute to the decrease in the total conductivity. This explains why the conductivity achieved for the HNO₃-treated TiO₂-added system is lower than the untreated TiO₂-added system.



Fig.4. Frequency dependence of dielectric constant, ε_r for H-chitosan/PS-LiCF₃SO₃ with a) untreated TiO₂ and b) HNO₃-treated TiO₂

The ac conductivity can be obtained from the dielectric constant, ε_r and loss tangent, tan δ according to the Equation (2)

$$\sigma_{ac} = \varepsilon_0 \varepsilon_r \omega * \tan \delta \tag{2}$$

where $\varepsilon_0 = 8.85 \times 10^{-14}$ F cm⁻¹. In general, the phenomena of the conductivity-frequency dispersion are analyzed using the Jonscher's universal power law as stated in Equation (3)

$$\sigma(\omega) = \sigma_{dc} + A\omega^s \tag{3}$$

where the dc conductivity, σ_{dc} is the frequency-independent component, A is a parameter dependent on temperature and s is the power law exponent with values in the range 0 < s < 1.0. $\sigma(\omega)$ is generally believed to reflect the mechanism of charge transport among charge carriers. The Jonscher universality is not limited to analyze the AC conductivity in glass but has been extended to study the ac conductivity of polymer electrolytes [16]. In order to understand the conduction mechanism, different models have been proposed to explain the AC conductivity [17]. These models are quantum mechanical tunneling (QMT), the correlated barrier hopping (CBH) and overlapping large polaron tunneling (OLPT) [18-19]. In the QMT model, the *s* is independent of temperature. In the CBH model, *s* decreases with increasing temperature. While, for the OLPT model, *s* decreases to a minimum value and increases again as temperature increases. Fig. 5 and 6 depict the plot of log [$\sigma(\omega)$ - σ dc] versus log ω at various temperatures for untreated TiO₂ and HNO₃-treated TiO₂. Values of exponent *s* can be evaluated from the slope of each plots.



Fig.5. Plot of log $[\sigma(\omega) - \sigma_{dc}]$ versus log ω for a) 4 wt.% and b) 6 wt.% HNO₃-treated TiO₂ at different temperatures

Fig. 6 shows the variation of exponent *s* with temperature for both treated and untreated sample containing 4 and 6 wt.% TiO₂. It can be observed that the power law exponent s for 4 wt.% and 6 wt.% untreated TiO₂ and HNO₃-treated TiO₂ decreases continuously with increasing temperature. Thus, the conduction mechanism for both electrolytes the systems can be interpreted as the correlated barrier hopping (CBH) model which means that the ions hop over a barrier between two complexation sites. According to [20], conduction mechanism for

electrolytes chitosan doped silver triflate (AgCF₃SO₃) also follows the CBH model below 358





Fig.6. Variation of exponent s with temperature for a) untreated TiO_2 and b) HNO₃-treated TiO_2

3. EXPERIMENTAL

H-chitosan prepared by acyl modification technique and used tetrahydrofuran (THF) as the media. Details of H-chitosan preparation were described in this paper [8]. LiCF₃SO₃ from Acros Organics were dried at 100°C for 24 hours prior to use. TiO₂ powder with particle size of 30-40 nm obtained from Nanostructured and Amorphous Material Inc. were used as the inorganic filler. TiO₂ was acid-treated by stirring in diluted HNO₃ solution (0.83 v/v %) for 8 hours at 80°C, rinsed with de-ionized water until the filtrates were neutralized and then dried for 12 hours at 100°C.

Films of H-chitosan/PS blend were prepared by solution casting technique. The two polymers

were first dissolved separately in an appropriate amount of THF. Then, the required amounts of LiCF_3SO_3 and TiO_2 were added. The resulting mixture was then stirred at room temperature until complete dissolution and homogenous. The solution obtained were cast in glass petri dishes and allowed to completely evaporate slowly at room temperature to form films. The films were kept in a desiccator for continuous drying.

In order to investigate the structure of polymer electrolyte films, XRD scans was taken using X-Pert PRO XRD which employs Cu-K α X-radiation of wavelength $\lambda = 1.5418$ Å between a 2 θ angle of 5° to 80°. The impedance measurement of the films was carried out using HIOKI 3532-50 LCR Hi Tester in the frequency range of 100 Hz to 1 MHz and in the range of temperature from 283 to 333 K. The prepared electrolyte film was sandwiched between two stainless steel electrodes with diameter 2.5 cm under spring pressure. The ionic conductivity, σ of the sample was calculated using Equation (1).

$$\sigma = \frac{t}{R_b A} \tag{4}$$

where t is the sample thickness, A is the effective contact area and R_b is the bulk resistance which can be obtained from the complex impedance plot.

4. CONCLUSION

The effect of treated and untreated TiO₂ on the structural and electrical properties of CPE H-chitosan/PS-LiCF₃SO₃. XRD results revealed the crystallinity of the H-chitosan/PS decreased as both types of TiO₂ added in the CPE up to maximum amount, which are 4 % for treated TiO₂ and 6 wt.% of treated TiO₂. Beyond this composition of TiO₂, the crystallinity of H-chitosan/PS increased significantly. The variation in conductivity followed the trend of crystallinity fraction, which optimum ionic conductivity can be observed at 4 wt. % for treated TiO₂ and 6 wt.% of treated TiO₂ systems. The difference in conductivity with varying TiO₂ content also be understood on the basis of free ion concentration as reflected in the variation in dielectric constant. The ac conductivity for H-chitosan/PS-LiCF₃SO₃-TiO₂ and H-chitosan/PS-LiCF₃SO₃-HNO₃-treated TiO₂ electrolyte systems follows the Jonscher's universal power law. From this law, we concluded that the conduction mechanism for these CPE systems can be interpreted based on the CBH model.

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