MODELLING EFFLUENT ASSIMILATIVE CAPACITY OF IKPOBA RIVER, BENIN CITY, NIGERIA

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ABSTRACT
The sheer display of reprehensible propensity on the part of public hospitals, abattoirs, breweries and city dwellers at large to discharge untreated waste, debris, scum and, in particular, municipal and industrial effluents into Ikpoba River has morphed into a situation whereby the assimilative capacity of the river has reached a record level. The seeming quietism and clinical posture of the relevant Environmental Agency to this pathological condition is sickening and in any case seen as remiss on their part. This paper seeks to determine the assimilative capacity of the river with a view to articulating policy-proposal stream in the instance that its value is unsafe for ichthyofaunal beings and humans. A combination of basic Streeter-Phelp equation and monograph of Fair et al. were used for the determination of the assimilative capacity and the maximum allowable biological oxygen demand (BOD) load discharged into the river from three identified point sources of wastewater and for three different seasons in Nigeria (i.e. rainy, dry and harmattan seasons). Results indicate that in all the segments studied, the Fair ratio (self-purification factor) is less than unity, indicating the predominance of deoxygenation rate over reaeration rate. Reaeration rate ranges over all real values from 0.641day⁻¹ to 0.693day⁻¹, while deoxygenation rate ranges between 0.718 day⁻¹ and 0.839 day⁻¹; a condition which indicates a poor assimilative capacity potential. Moreover, a higher assimilative capacity was obtained for rainy season for all the segments studied, with sampling point 3 (Guinness-harmattan and dry season) showing an overall worse assimilative capacity and poor maximum allowable BOD of 8.1x10⁹, 1.28x10⁹ and 5.60x10⁹ kg/day respectively. In a way, the determination of the assimilative capacity of Ikpoba River is a landmark in the history of the river pollution. It begs belief that we live down the narrowing pathological condition of the river without recognizing its wider implications.

Keywords: Assimilative capacity, Fair ratio, untreated waste, pathological condition, maximum allowable BOD load

1. INTRODUCTION
Effluent plumes, municipal wastes, scum, and surface runoffs are often channeled into rivers, especially in developing countries where laws on environmental regulation are not strictly enforced [1]. These loadings in the river deplete its dissolved oxygen (DO) leading to the development of a long stretch of dissolved oxygen (DO) sag zone that is detrimental to aquatic lives. Besides depletion of DO, river pollution appears to be associated with spread of water borne diseases. River water serves several purposes to communities settling around its course such as agricultural, industrial and domestic utilities. Thus, river pollution beyond its assimilative capacity is quite expensive to treat in order for it to meet the aforementioned needs of the communities. It is therefore important that assimilative capacity of surface flowing water bodies be determined. Further, in order to articulate and develop a reliable water quality management programme for a polluted water body, a sound understanding of the correlation between the waste discharge into it and its capacity to assimilate same without compromising its original water quality is necessary. This can provide more logical ground for water quality regulation for the particular river rather than working on a more general and uniform rules

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which may not be applicable to every water body within the jurisdiction of the regulatory body. It is therefore imperative that this study be carried out on Ikpoba River, Benin city, Nigeria which has been severally confirmed to be polluted [2-5].

While a number of studies have expressed concern about the polluted status of Ikpoba River and addressed various aspects of its pollution status, albeit with hardly appropriate analytics, the mechanics of the gradual development of its assimilative capacity has, to the best our knowledge, been rarely explored. The study [6] provides some insight regarding the need for urgent proactive measures to forestall imminent epidemic arising from the effects of pollution on the river. The assessment of the assimilative capacity of a river is necessary before any efficient management programme of the river can be developed [7].

The pioneering work of [8] which investigates the relationship between dissolved oxygen (DO) resources and the measured organic waste decay giving rise to biochemical oxygen demand (BOD) from which the classic dissolved oxygen sag model was produced, has been very pivotal in the analysis and determination of capacity of streams to assimilate pollution of organic wastes. Since the classical theory of [8], many investigators have applied the theory to water quality management studies and several modifications as well had been proposed for various scenarios [9-14]. Deserving of note are the works [15-18] which claim that apart from the biochemical oxidation of organic matter and atmospheric reaeration of river water, there are other factors in a water body which affect the DO-BOD relationship. According to them these factors are:

i. removal of oxygen by respiration of plankton and rooted plants;
ii. removal of oxygen from water by purging action of gases rising from benthal layer;
iii. removal of oxygen from water by diffusion into the benthal layer to satisfy oxygen demand in the aerobic zone of this layer;
iv. removal of BOD by sedimentation and adsorption;
v. addition of BOD by local runoff;
vi. addition of BOD along a river stretch by scour of bottom deposits or diffusion of partly decomposed organic products from the benthal layer into the waters above;

vii. addition of oxygen by photosynthetic action of plankton and fixed plants; and
viii. continuous redistribution of BOD and DO by the effect of longitudinal dispersion.

Over the years, several efforts had been made to produce several complex water quality models which tend to describe the changes in dissolved oxygen (DO) as occasioned by changes in BOD. Examples of such complex models are QUAL 2E by [19] and WASP 6 by [20]. The foregoing notwithstanding, however, the classic study [8] and its various modifications have remained the most widely used set of models [14]. The study [21] suggests that effective water management program should use models which are easily interpretable by decision makers. The current study has therefore applied basic Streeter–Phelps model to determine the assimilative capacity of Ikpoba River. This study therefore seeks to investigate the dynamics of evolution of assimilative capacity and the maximum allowable BOD of the river under the existing effluent discharge into it. The findings will provide a guide towards a pragmatic approach in maintaining water quality standards for water quality managers and regulatory bodies.

2. MATERIALS AND METHODS

2.1 Study Site

Ikpoba River is located in Benin City, Nigeria (Figure 1). As can be seen from the figure, the river flows from top to bottom of the map, traversing the points P1, P2, P3 and P4 which are the effluent discharge points, where samples were taken for the study. It navigates the city, flowing from North to South. Due to immense direct effluent loading of industrial effluents, domestic and agricultural activities, runoffs from municipal sewage system as well as the discharge of diverse abattoir wastes into the river, its water quality has been profoundly impaired.

The current study investigates the stretch of the river which is sandwiched between a public health institution whose wastes leach into the river and some large breweries which also channel their effluent discharge into it. Also, along the river bank of this reach is located a public abattoir which discharges diverse abattoir wastes, including cow blood and excreta. This stretch is estimated to be about 10km.
2.2 Sampling Design and Measurements

It has been established that velocity, depth, temperature and discharge are among the natural factors affecting the assimilative capacity of water bodies [22]. Based on this premise therefore, at each sampling station, Swoffer® meter was used to determine the speed of the river. Depth was taken at the various sampling points as well using Speedtech® depth sounder, while the temperature of the samples were taken in situ using mercury-in-glass thermometer (0-100°C). The cross-section of the river was measured by stretching a tape across its width. The river water samples for physiochemical, microbiological and heavy metal analysis were collected from four predetermined points. At each point, upstream and downstream, the samples for physiochemical and microbiological analyses were collected with 50ml reagent bottles which were washed with distilled water and further rinsed with water collected at the sample point before the collection of samples. Oxygen fixation for the specimens was done with Winkler solutions A and B. Distilled-water-diluted nitric acid was required to maintain the oxidation state of the elements and also to prevent materials from adhering to the walls of the container. The samples meant for heavy metal analyses were collected with 1 litre plastic container. These were done in June and December 2012 (i.e. raining season and dry season respectively). Upon handing over the samples to the personnel of the laboratory where the analyses were carried out they removed the samples from the ice chest and had them frozen prior to subsequent chemical analysis in line with fundamentals of field studies. All the water quality parameters were analyzed using appropriate standard methods namely APHA, HATCH Digital titration and Determination Bacteriology as specified in [23-25]. All the laboratory analyses were done in Earth Quest International Limited, Warri, Nigeria.

2.3 Method of analysis of Data

In this study, the maximum $\text{BOD}_u$ load into the river and its assimilative capacity were determined by a
combination of the basic Streeter-Phelps equation and the monograph of Fair et al. This is based on the fact that the prime indicator of water quality of a river is its DO level. So the impact of BOD on DO was investigated. The basic Streeter-Phelps equation was considered adequate for this analysis due to its long history of use, ease of computation, wide acceptability and applicability in spite of its short comings particularly the assumption of steady state assimilation of the pollution load. Moreover, according to [26], there are no effective alternative formulations with superior range of conditions.

2.3.1 DO Saturated Value
The calculation of the DO saturation value ($C_s$) for various water temperatures as introduced by [27] is made feasible by the use of the following empirical equation:

$$C_s = 14.541233 - 0.3928026T + 0.00732326T^2 + 0.00006629T^3$$

(1)

2.3.2 Reaeration Rate Constant ($K_2$)
According to study [28], the reaeration rate constant ($K_2$), which is a function of the diffusivity of oxygen in water, depth of river, velocity of river, and temperature of river, can be calculated with equation (2) that follows, which is generally applicable to streams with a depth of greater than 1.52 meters. This makes it applicable to the current study. In that regard, it is justifiable to apply the equation to this case study as follows [28]:

$$K_2(T) = 3.93V^\frac{1}{2}(1.024)^{(T-20)}$$

(2)

where 3.93 is the diffusivity of oxygen in water, $H$ is the average depth in metres, $V$ is the Flow velocity in ms$^{-1}$, and $T$ is the temperature in degree Celsius.

2.3.3 Deoxygenation Coefficient ($K_1$)
Also, according to [28] the deoxygenation coefficient ($K_1$) is calculated with the formula [28]:

$$K_1(T) = 3.93V^\frac{1}{2}(1.048)^{(T-20)}\frac{1}{H^2}$$

(3)

The critical DO deficit,

$$D_c (mg/l) = C_s - C_e$$

(4)

Figure 2: The monograph of allowable BODu loading of the receiving waters, [29].
The capacity of a river to oxidize organic wastes is determined by its oxygen dynamics as described by the study [7] in the following equation:

\[ D_{0} = S - C \]  

where \( S \) is the initial dissolved oxygen (DO) content starts to diminish with initial deficit \( D_{0} \) and continues up to a certain distance downstream when it begins to recover. This variation of dissolved oxygen deficit with the distance downstream vis-à-vis the time of flow from the point of pollution is illustrated by the oxygen sag curve (Figure 2).

The point of minimum DO, being the maximum deficit, which is also called the critical deficit \( D_{c} \), is the point of inflexion of the curve. It is considered the major point of the oxygen sag analysis.

The capacity of a river to oxidize organic wastes is determined by its oxygen dynamics as described by the study [7] in the following equation:

\[ D = S - C \]  

where \( S = \text{DO deficit} \) and \( C = \text{DO in Water} \) i.e.

\[ D_{c} = C_{c} - C_{a} \]  

where \( C_{a} \) is the initial dissolved oxygen concentration (prior to discharge point)

**Self-purification factor:**

\[ (f) = \frac{k_{2}}{k_{1}} \]  

\[ L_{a} / D_{c} \] ratio, obtained from the monograph of Fair et al. as a function of purification factor \( f \) and the ratio \( D_{a} / D_{c} \)

\[ L_{a} = D_{c} \left( L_{a} / D_{c} \right) \]  

where \( B_{a} \) is the maximum allowable BOD load discharge at the river and it was calculated with the relationship:

\[ B_{a} = 24 \times 3600 \times \left( Q_{r} + Q_{w} \right) L_{a} - Q_{L_{p}} / 1000 \]  

where \( Q_{r} \) is the river flow rate; \( Q_{w} \) is the discharge flow rate

Assimilative Capacity (AC) was calculated with relationship:

\[ AC = 24 \times 3600 \times L_{a} \times Q_{r} / 1000 \]  

**3. THEORETICAL CONCEPT**

Every fresh water body has saturated dissolved oxygen which is a function of its ambient temperature and total dissolved salt present in it [31]. When a river with initial saturated dissolved oxygen \( D_{0} \) is polluted, the dissolved oxygen (DO) content starts to diminish with initial deficit \( D_{0} \) and continues up to a certain distance downstream when it begins to recover. This variation of dissolved oxygen deficit with the distance downstream vis-à-vis the time of flow from the point of pollution is illustrated by the oxygen sag curve (Figure 2).

The point of minimum DO, being the maximum deficit, which is also called the critical deficit \( D_{c} \), is the point of inflexion of the curve. It is considered the major point of the oxygen sag analysis.

The capacity of a river to oxidize organic wastes is determined by its oxygen dynamics as described by the study [7] in the following equation:

In terms of the deficit with time, DO deficit= saturated DO - DO in Water i.e.

\[ D = S - C \]  

where \( Z = L e^{-K_{1} t} \) is the critical dissolved oxygen concentration.

Substituting and integrating yields the following equations, referred to as the basic Streeter-Phelps equations

\[ D_{t} = \frac{K_{1} L_{o} e^{-K_{1} t}}{K_{2} - K_{1}} (e^{-K_{1} t} - e^{-K_{2} t}) + D_{0} e^{-K_{2} t} \]  

\[ \frac{dD_{a}}{dt} = \frac{K_{1} L_{o} e^{-K_{1} t}}{K_{2} - K_{1}} - K_{2} D_{a} = 0 \]  

\[ D_{0} = \frac{K_{1}}{K_{2}} L_{o} e^{-K_{1} t} \]  

\[ t_{c} = \frac{1}{K_{2} - K_{1}} \ln \left( \frac{K_{2}}{K_{1}} \right) \left( 1 - D_{0} \frac{K_{2} - K_{1}}{K_{1} L_{o}} \right) \]

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\[ t_{c} = \frac{1}{K_{2} - K_{1}} \ln \left( \frac{K_{2}}{K_{1}} \right) \left( 1 - D_{0} \frac{K_{2} - K_{1}}{K_{1} L_{o}} \right) \]

In the above equations, \( D_{t} \) = DO deficiency at any point in time (mg/l), \( K_{1} \) is the oxygen consumption coefficient to base \( e \) (per day), \( K_{2} \) is the reaeration rate constant to base \( e \) (per day), \( L_{o} \) is the initial BOD load (mg/l), \( D_{0} \) is the initial DO deficiency and \( t \) is the time of travel (day) as \( t = \frac{x}{v} \) in which \( x \) is the distance from the upstream point of discharge; \( v \) is the velocity (m/day) and \( (t_{c}, D_{c}) \) is critical point at which the rate of change of DO equals zero during downstream movement.

**4. RESULTS AND DISCUSSION**

**4.1 Assimilative Capacity**

The self-purification factors used in this study are the deoxygenation rate coefficient \( (K_{1}) \) and the reaeration rate coefficient \( (K_{2}) \). These were used to determine the Fair ratio \( f = \left( \frac{K_{1}}{K_{2}} \right) \). The Fair ratio depicts the degree of preponderance of reaeration over deoxygenation [32]. The results in Table 1 which was obtained by the method of [30] show that the reaeration rate ranges between 0.641day\(^{-1}\) and 0.693day\(^{-1}\) for different segments of the river, and for the different seasons considered, while the deoxygenation rate ranges from 0.718day\(^{-1}\) to 0.839day\(^{-1}\).

The Fair ratio \( f \) is less than unity in all of the segments of the river studied and for all of the seasons. The import of this is that deoxygenation predominates reaeration in the stretch of the river studied. Furthermore, it can be seen from the results in Table 1 that the assimilative capacity and the maximum allowable BOD are higher during the rainy season for all the segments studied. This conforms to reality consequent upon dilution factor. The rainy season provides the river with sufficient water for dilution. This makes the DO level to be farther away from the critical point due to the availability of
relatively sufficient DO in the river before the introduction of the wastewater. Therefore, the assimilative capacity in the rainy season is increased. Again, at sampling point 3, results reveal that the maximum allowable BOD are 7.39x10^9, 1.28x10^10 and 1.07x10^10 kg/day were obtained for the aforementioned three different seasons respectively at sampling point 3. It is obvious therefore that there is an urgent need for relevant regulatory bodies like The Nigeria Environmental Standard and Regulations Enforcement Agency (NESREA) to weigh in with strict enforcement of existing regulatory laws to forestall an epidemic.

**Figure 2.** Deoxygenation, reoxygenation and oxygen Sag curve.

\[ D = C_a - C_o \]

\[ D_o = D_t - C_t \]

\[ D_t = C_a - C_o \]

where: \( D = \) dissolved oxygen deficits in mg/l, \( C_a = \) saturated concentration of dissolved oxygen in mg/l, \( C_o = \) actual concentration of dissolved oxygen in mg/l, \( D_o = \) initial DO deficit in mg/l which is DO deficit at \( t = 0 \), \( D_t = \) critical DO deficit in mg/l, \( C_s = \) critical DO, in mg/l.

**Table 1. Water Quality Determinants for Ikpoba River by Seasons**

<table>
<thead>
<tr>
<th>Input/output data</th>
<th>Symbol</th>
<th>Unit</th>
<th>UBTH Dry Season</th>
<th>UBTH Harmattan season</th>
<th>UBTH Rainy season</th>
<th>EWAH RD. JUNCTION Dry season</th>
<th>EWAH RD. JUNCTION Harmattan season</th>
<th>EWAH RD. JUNCTION Rainy season</th>
<th>GUINNESS Dry season</th>
<th>GUINNESS Harmattan season</th>
<th>GUINNESS Rainy season</th>
</tr>
</thead>
<tbody>
<tr>
<td>Temperature of river</td>
<td>( T )</td>
<td>°C</td>
<td>23.6</td>
<td>25.2</td>
<td>22.6</td>
<td>26.8</td>
<td>27.5</td>
<td>25.9</td>
<td>28.2</td>
<td>27.0</td>
<td>25.9</td>
</tr>
<tr>
<td>Initial DO prior to discharge point</td>
<td>( C_a )</td>
<td>mg/l</td>
<td>7.9</td>
<td>7.6</td>
<td>8.5</td>
<td>7.0</td>
<td>6.6</td>
<td>7.4</td>
<td>7.1</td>
<td>6.8</td>
<td>7.8</td>
</tr>
<tr>
<td>DO after discharge</td>
<td>( D_t )</td>
<td>mg/l</td>
<td>7.8</td>
<td>7.6</td>
<td>7.8</td>
<td>6.7</td>
<td>6.2</td>
<td>6.2</td>
<td>6.0</td>
<td>0.2</td>
<td>0.6</td>
</tr>
<tr>
<td>Critical DO</td>
<td>( C_s )</td>
<td>mg/l</td>
<td>5.0</td>
<td>5.0</td>
<td>5.0</td>
<td>5.0</td>
<td>5.0</td>
<td>5.0</td>
<td>5.0</td>
<td>5.0</td>
<td>5.0</td>
</tr>
<tr>
<td>Saturated DO</td>
<td>( C_r )</td>
<td>mg/l</td>
<td>8.47</td>
<td>8.23</td>
<td>8.63</td>
<td>8.0</td>
<td>7.9</td>
<td>8.1</td>
<td>7.8</td>
<td>8.0</td>
<td>8.1</td>
</tr>
<tr>
<td>( D_t = C_r - C_s )</td>
<td>( D_c )</td>
<td>mg/l</td>
<td>3.47</td>
<td>3.32</td>
<td>3.36</td>
<td>3.0</td>
<td>2.9</td>
<td>3.1</td>
<td>2.8</td>
<td>3.0</td>
<td>3.1</td>
</tr>
<tr>
<td>Decay rate constant at T°C</td>
<td>( K_{(T)} )</td>
<td>day⁻¹</td>
<td>0.785</td>
<td>0.727</td>
<td>0.718</td>
<td>0.785</td>
<td>0.810</td>
<td>0.753</td>
<td>0.83</td>
<td>0.790</td>
<td>0.753</td>
</tr>
<tr>
<td>Reaeration rate T°C</td>
<td>( K_{(T)} )</td>
<td>day⁻¹</td>
<td>0.671</td>
<td>0.645</td>
<td>0.641</td>
<td>0.671</td>
<td>0.680</td>
<td>0.665</td>
<td>0.693</td>
<td>0.67</td>
<td>0.659</td>
</tr>
<tr>
<td>BODs (river water)</td>
<td>( L_r )</td>
<td>mg/l</td>
<td>4.1</td>
<td>3.10</td>
<td>3.4</td>
<td>0.6</td>
<td>0.8</td>
<td>1.3</td>
<td>1.1</td>
<td>1.3</td>
<td>1.5</td>
</tr>
<tr>
<td>River flow rate</td>
<td>( Q_r )</td>
<td>m³/day</td>
<td>13996800</td>
<td>25292000</td>
<td>15246100</td>
<td>13996800</td>
<td>25292000</td>
<td>15246100</td>
<td>13996800</td>
<td>13996800</td>
<td>15246100</td>
</tr>
<tr>
<td>Discharge flow rate</td>
<td>( Q_d )</td>
<td>m³/day</td>
<td>2160000</td>
<td>1728000</td>
<td>2160000</td>
<td>2160000</td>
<td>1120000</td>
<td>1120000</td>
<td>6200000</td>
<td>4160000</td>
<td>1728000</td>
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<tr>
<td>Self-purification factor</td>
<td>( f )</td>
<td></td>
<td>0.85</td>
<td>0.89</td>
<td>0.89</td>
<td>0.85</td>
<td>0.84</td>
<td>0.87</td>
<td>0.83</td>
<td>0.85</td>
<td>0.87</td>
</tr>
<tr>
<td>( D_s / D_o )</td>
<td>( D_i / D_c )</td>
<td></td>
<td>0.16</td>
<td>0.2</td>
<td>0.04</td>
<td>0.33</td>
<td>0.45</td>
<td>0.23</td>
<td>0.25</td>
<td>0.4</td>
<td>0.1</td>
</tr>
<tr>
<td>( L_a / D_c )</td>
<td>( L_i / D_c )</td>
<td></td>
<td>2.5</td>
<td>2.3</td>
<td>2.7</td>
<td>2.5</td>
<td>1.9</td>
<td>2.6</td>
<td>2.4</td>
<td>1.9</td>
<td>2.6</td>
</tr>
<tr>
<td>( L_a )</td>
<td>( L_i )</td>
<td>mg/l</td>
<td>8.7</td>
<td>8.7</td>
<td>9.8</td>
<td>7.5</td>
<td>4.6</td>
<td>8.1</td>
<td>6.7</td>
<td>5.7</td>
<td>8.1</td>
</tr>
<tr>
<td>Maximum allowable BOD</td>
<td>( B_a )</td>
<td>Kg/day</td>
<td>5.7x10^9</td>
<td>4.4x10^10</td>
<td>6.5x10^10</td>
<td>5.8x10^9</td>
<td>2.2x10^9</td>
<td>6.2x10^9</td>
<td>7.3x10^9</td>
<td>5.6x10^9</td>
<td>1.05x10^10</td>
</tr>
<tr>
<td>Assimilative capacity (AC)</td>
<td>( AC )</td>
<td>Kg/day</td>
<td>1.05x10^10</td>
<td>1.95x10^10</td>
<td>1.29x10^10</td>
<td>9.07x10^9</td>
<td>1.03x10^10</td>
<td>1.07x10^10</td>
<td>8.1x10^9</td>
<td>1.28x10^10</td>
<td>1.07x10^10</td>
</tr>
</tbody>
</table>
An earlier study by the authors [33] analysed the relationship between the heavy metals and the other pollution determining parameters. It was discovered that heavy metals, namely Cadmium (Cd), Copper (Cu), Iron (Fe) and Lead (Pb) correlate negatively with pH and DO on the one hand but positively with BOD, COD and Fecal coliform on the other. One possible interpretation of this correlation is that the presence of heavy metals tends to cause oxidation reaction that depletes dissolved oxygen (DO) in the river. Therefore the more the heavy-metal-bearing effluents are injected into the river, the more the abundance of Feacal coliform, COD, and BOD. As the loading abates, so do the Feacal Coliform, BOD and COD proportionately decrease. In other words, there is positive correlation between heavy metals BOD, COD and Fecal Coliform. However, the reverse is the case for correlation between heavy metals on the one side and pH and DO on the other. This latter case involves inverse relationship in the sense that the more the heavy metals which come from effluent loading, the more the oxidation reaction that depletes the DO. The discernment of this relationship was made possible by the correlation analysis statistical methodology applied in the study under reference.

4.2 Articulation of Policy Proposal
Pollution, arising from urbanization and industrialization around a segment of Ikpoba River, has morphed into an unhealthy ecosystem capable of causing an epidemic [33]. The assimilative capacity which is an index of the level of the perceived pollution is about 8.1x10^9 kg/ day^-1 within associated maximum allowable BOD of 1.02x10^9 kg/day^-1 derived from sample observation of 16.2 mg/l for station 3 downstream. This value, although considered to be still within limits of maximum allowable for Nigeria (see table on appendix for more details) needs to be put in check to avoid escalation. Moreover, there is pronounced oxygen sag at station 3 downstream giving a least value of 0.2mg/l as against acceptable value of 5mg/l [34]. This development causes serious degradation of assimilative capacity in the river portion under reference. Our results show that the river tends to recover from the oxygen sag effects (sharp decrease in DO and hence degraded assimilative capacity) after some 200m downstream and these figures are considered quite unsafe. Following the finding from this study, the following recommendations are suggested.

5. RECOMMENDATIONS:
1. Individuals and corporate organisations found to be committing infractions of the existing regulatory environmental laws should be prosecuted to serve as deterrent to others. There has not been any recorded case of offenders being prosecuted.
2. Although existing regulations require that industrial effluents should be treated before being discharged into the river, it has been an exception rather than the rule. Environmental laws should be made enforceable.
3. The foregoing problem-solution stream is hereby proposed as policy agenda for Nigeria Environmental Standard and Regulations Enforcement Agency (NESREA).

6. CONCLUSION
The objective of this study was to determine the assimilative capacity and the maximum allowable BOD discharge onto the urbanized portion of Ikpoba River which has been inundated with diverse industrial effluents and municipal wastewater discharge. The results show that the deoxygenation rate in the river dominates oxygenation rate, thus portraying the river as highly polluted with poor assimilative capacity potential. Furthermore, for each of the segments studied, rainy season shows a higher tendency for minimum acceptable dissolved oxygen concentration than both the dry and harmattan seasons.

The objectives of this study, as stated earlier, were therefore fully realized having successfully determined the assimilative capacity and the maximum allowable BOD discharge in the reach of the river studied. It is therefore hoped that this work provides needed scientific and empirical basis for Nigeria Environmental Standard and Regulations Enforcement Agency (NESREA), stakeholders and decision makers in general for decisions concerning the water quality problems and surveillance programmes and other regulatory activities on surface water in general and Ikpoba River in particular.

7. REFERENCES
Industry and Energy Division. 1st Edn. West Central Africa Department, Annexes pp 60-62


35. M. Bosnic, J. Buljan(2000). Limits for discharge into water bodies and sewers US/RAS/92/120 Regional Programme for Pollution Control in the Tanning Industry in South-East Asia UNIDO publication


38. FEPA (1990) *Interim Guidelines and Standards for Environmental Pollution Control in Nigeria*


APPENDIX: COMPARATIVE LIST OF EFFLUENT STANDARDS FOR DIFFERENT COUNTRIES OF THE WORLD

<table>
<thead>
<tr>
<th>S/N</th>
<th>COUNTRY</th>
<th>BOD mg/l</th>
<th>COD mg/l</th>
<th>pH</th>
<th>SOURCE</th>
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<tr>
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<tr>
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<tr>
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